

**APPLICATION FOR  
U.S. LETTERS PATENT**

**by**

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**for**

**HETERODYNE INTERFEROMETRY FOR  
SMALL SPACING MEASUREMENT**

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## HETERODYNE INTERFEROMETRY FOR SMALL SPACING MEASUREMENT

### Field of the Invention

This present invention relates to high-speed, high precision measurement of  
5 the distance between two near contact surfaces one of which is an optical  
transparent element. In particular the invention relates to an apparatus and method  
for performing this measurement using a heterodyne interferometer. Moreover,  
this invention relates to an optical interferometer for measuring the flying height  
of a magnetic head.

### 10 Background of the Invention

In magnetic data storage, there is a requirement for measuring the flying  
height of the slider assembly which is in near contact with a high-speed rotating  
disk in order to optimize the performance of the slider assembly. The flying  
height is the distance between the magnetic head pole and the surface of the  
15 rotating magnetic disk. Recently, the rapid increase in recording density has  
caused a continuous reduction in the flying height. The flying height is generally  
less than 250nm depending on the design of the slider. The trend is toward an  
ultra-low flying height which is less than 25nm.

Optical Flying Height Testing (OFHT) is the most popular testing  
20 technique in the field. OFHT are almost invariably based on interferometry.  
There are two known methods. The first method is measuring the flying height  
from a real magnetic disk through the backside of the slider. The second method  
is measuring the disk-slider spacing directly, using a transparent disk to replace  
the magnetic disk. The first method is not popular due to the fact that the

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accuracy of the measurement depends on the uniformity of the thickness of the slider. Moreover, the backside of the slider is not accessible on most production slider assemblies. Currently, the second method is more widely used in commercial applications.

5 Until now, there were three types of interferometry developed for flying height testing. The three types include white light interferometry, three-wavelength interferometry, and monochromatic interferometry. With a white light interferometer, a flying height of 700 to 300nm can be detected accurately. 10 Three-wavelength interferometer is an extension of white light interferometer. A flying height of less than 250nm can be measured with a three-wavelength interferometer with acceptable errors. Both a white light interferometer and a three-wavelength interferometer are subject to multi-reflections in the disk-slider air bearing, which produces errors. When the flying height is reduced to 50nm, 15 the error caused by multi-reflections cannot be neglected. Therefore, the polarization interferometer was developed to measure ultra-low flying height.

In U.S. Patent 4,606,638, Sommargren proposed a polarization phase modulated Fizeau interferometer in which the reference surface is the front surface of a plate polarizer. The modulated interference pattern is detected by a CCD array. The signal provides the absolute distance between the reference surface and 20 the flying slider. Although this technique was an advance in providing the flying height, pitch angle and roll angle in a single measurement, it is not practicable because the measurement accuracy is dependent on the flatness of the glass disk surface which acts as a plate polarizer.

25 In U.S. Patent 5,218,424, Sommargren proposed a polarization interferometer. In a polarization interferometer, a coherent, single wavelength, linearly polarized beam passes through a phase shifter which varies the relative phase of the orthogonal polarization components of the beam by 0,  $\pi/2$ ,  $\pi$ ,  $3\pi/2$ . Then the beam is directed to the glass disk at a Brewster's angle. The polarized beam P will pass through the glass disk and strike the slider without being

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reflected from glass disk surface. While the S polarized beam will be reflected by each glass-air interface. Therefore, the S polarization beam can be used as the reference beam and the phase difference between S and P polarization beams carries the flying height information. The phase change which is caused by the  
5 optical path difference between S and P polarization beams, therefore, can be determined by a four-step algorithm. By using the polarized laser beam, the error caused by multi-reflection is completely eliminated. Thus, the apparatus is capable of measuring extremely small gaps. Despite the advantage, this technique has some significant limitations, including the use of a very expensive  
10 complicated, high speed phase modulator. Moreover, the data processing rate is quite slow, around 15HZ, which is not suitable for commercial applications.

In U.S. Patent 5,660,441, Groot proposed a quad-beam polarization interferometer. Three of the four beams are S polarization, the other one is a P polarization. These four beams are parallel to each other and are directed to the  
15 glass disk at Brewster's angle. Except for the P polarized beam passing through glass disk without reflection, all the beams are reflected back from the surface of the glass disk. After being reflected from the slider ABS, the P polarized beam again passes through the glass disk. The two reflected S polarized beams are made to interfere thereby providing a reference. The P polarized beam is made to  
20 interfere with the remaining S polarized beam. Thus, the interfered beam contains the flying height information. The spacing between disk surface and slider ABS can be detected by comparing the two interfered beams. The main advantage of this technique is that it eliminates the phase modulator which was used by all the prior-art techniques. Therefore, the signal-processing rate can be very fast, and  
25 the error introduced by the phase shifting can be eliminated. This apparatus is capable of measuring ultra-low flying height with the required accuracy. In U.S. Patent 5,751,427, Groot further improved his polarization interferometer by using a single linearly polarized beam.

All these prior art techniques are based on homodyne interferometry, using phase measurement to find out the flying height by detecting the optical path difference between reference beam and measurement beam. One phase measurement method, which is generally employed in all these prior art

5 techniques, is the four-step algorithm. This method is subject to the intensity variation of the laser beam, which may be caused by an unstable laser source, birefringence of the high-speed rotating glass disk, disturbances from the surroundings, etc. Moreover, the reflection of the slider ABS will introduce a phase change in the measurement beam which strikes it. In the prior art

10 technique, this phase change was assumed to be  $\pi$ . These will cause flying height measurement errors as large as 10nm. It is acceptable when the flying height is above 250nm. When flying height is reduced to less than 50nm, it is necessary to precisely measure the phase change introduced by the ABS reflection. Usually, the correction of the phase change occurring at the ABS will be done by a

15 measurement instrument independent of the flying height tester which is called an ellipsometer. The correction of the ABS reflection phase change is substantial disadvantage of all the prior art techniques. Although Groot integrated the ABS reflection phase change correction with the flying height testing into one instrument in his U.S. Patent 5,757,427, the correction is still a separate

20 measurement step that has to be done before the gap measurement.

### **Summary of the Invention**

Thus, the objective of the present invention is to provide an apparatus and method capable of measuring the flying height by removing various uncertainties in an OFHT using heterodyne interferometry without requiring any extra

25 measurement other than flying height testing. The embodiment of the present invention has a laser source emitting two orthogonally polarized beams of different frequency by using a Zeeman laser source or by using an acousto optic modulator and recombining the beam by using optical components. The beam is spatially

filtered and expanded in diameter by using a spatial filter, by using a pinhole, or with optical fibers. The beam is made to strike the object at a single point or to scan on the object by using acousto optic deflector. The embodiment of the present invention has means to obtain parallel scanning beam and to focus the

5 scanning beam on a single plane. The beam is divided in to two, one for the reference path and the other for the measurement path. The measurement beam strikes the glass disk at an oblique angle such that the P polarized beam refracts through the glass disk and is reflected from the surface of the object. The S polarization beam is reflected from the bottom surface of the glass disk. The

10 reflected S and P polarized beams from the bottom surface of the disk and the object surface are made to interfere on the measurement photo detector. The reference beams are made to interfere at the reference photo detector. Upon comparison of the phase change between the reference and the measurement signal, the displacement and the distance between the disk surface and the object

15 can be obtained using a phase meter and adopting heterodyne interfrometric principles. The reference signal can also be obtained by reflection from the surface of the object or the bottom surface of the glass disk by directing the beam at a particular oblique angle.

The second embodiment of the present invention is a means to measure an

20 object surface smaller than the focused spot size of the beam by using a diaphragm before the measurement photo detector to allow a smaller portion of the interfered beam to pass through it. The smaller the diameters of the diaphragm or slot results in a smaller object being measured in the focused spot size.

#### Brief Description of the Drawings

25 Figure 1 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a stationary measurement beam and a reference beam taken directly from light source.

Figures 2A and 2B are drawings showing setups to produce two orthogonally polarized beams with a frequency difference between them and to superimpose the two beams.

5 Figures 3A and 3B are drawings showing the optical setup and working principles of a spatial filter.

Figure 4 is a drawing illustrating the working principles of the preferred embodiment of the invention using a glass disk having polarization coating on its side closest to the object surface.

10 Figure 5 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a measurement beam and a reference beam which strike the bottom surface of the disk or the object surface at the same point but at a different angle.

15 Figure 6 is a drawing showing the working principles of the preferred embodiment of the invention when the measurement and reference beams strike the bottom surface of the glass disk or the object surface at the same point but at a different angle.

20 Figure 7 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a scanning measurement beam and a reference beam taken directly from the light source.

25 Figure 8 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a scanning measurement beam and scanning reference beam which strike the bottom surface of the glass disk or the object surface at the same point but at a different angle.

Figures 9A and 9B are drawings illustrating the working principles for obtaining a parallel scanning beam by using the combination of an acousto optic deflector, and focusing optics or scanning lens.

Figure 10 is a drawing illustrating the relative distance between optical components in the system.

Figure 11 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a collimated and stationary micro-sized measurement beam and a micro-sized reference beam taken directly from a light source.

Figure 12 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a collimated and stationary micro-sized measurement beam and a micro-sized reference beam which strike the bottom surface of the glass disk or the object surface at the same point but at a different angle.

Figure 13 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a collimated and stationary micro-sized scanning measurement beam and a micro-sized reference beam taken directly from the light source.

Figure 14 is a drawing showing a preferred embodiment of the invention setup to measure the distance of a flat object surface with respect to the surface of a rotating transparent disk using a collimated and scanning micro-sized measurement beam and a micro-sized reference beam, which strike the bottom surface of the glass disk or the object surface at the same point but at a different angle.

Figure 15 is a drawing showing the top view of the object with reference to the rotating glass disc.

Figure 16 is a drawing showing the method to measure the vibration of a smaller portion of the focused beam on the object by using a diaphragm or slit.

### Detailed Description of the Invention

Figure 1 shows a preferred embodiment of the invention employing an interferometric setup for measuring the distance of an object 28 surface that is nearly in contact with a surface 27 of a rotating transparent disk 25. The apparatus in this embodiment is preferably suited to the prediction of the aerodynamic flight characteristics of a conventional slider 28 over the surface of a rotating magnetic storage medium. A spindle drives disk 25. The size of the gap may be determined as a function of the speed of the rotating disk 25. The position of the test object 28 with respect to disk 25 may be further clarified by reference to Figure 15, which shows top a view of the disk 25, indicating the position of the object 28.

Referring to Figure 1, the laser beam is preferably obtained from the source 1, which provides a smooth laser beam 2 which contains two orthogonally polarized laser beams having a frequency difference between them. Source 1 can be of the type shown in Figures 2A or 2B, which will be explained in later sections. Non-polarization beam splitter 6 will split the beam 2 into two parts. The beam 15, the reference beam, passes through focusing lens 21 and interferes on passing through a polarizer or analyzer 22, falling on photodetector 23. The interferometric signal, reference signal 41 is sent into phasemeter 24. This optical path is used as a reference path for the flying height tester. The other optical path, which passes through beam splitter 6, is used as a measurement path. Focusing lens 7 focuses the wavefront 8 on to the air bearing surface (ABS) of the slider 28.

Figure 4 illustrates the working principles of the optical element 25. Optical element 25 is a transparent disk, which transmits wavefront 8. Surfaces 26 and 27 are plano and parallel. Surface 26 has an antireflection coating so that essentially all of plano wavefront 8 is refracted onto disk 25 and essentially none of wavefront 8 is reflected by the surface 26. Surface 27 of disk 25 is coated so that it is a surface polarizer. Therefore, when wavefront 8 is incident on the disk

surface at an oblique angle  $\theta$ , the surface 27 transmits the P polarization component and reflects the S polarization component of wavefront 8. Thus, surface 27 acts as the reference surface for the flying height tester. The S polarization wavefront reflected back by surface 27 passes through transparent disk 25 and is refracted by surface 26. The P polarization component of wavefront 8 is refracted by surface 27 and falls on the air bearing surface (ABS) of the slider 28. It is then reflected back from the ABS, goes through transparent disk 25 and is refracted by surface 26.

Referring to Figure 5, since the disk-slider spacing is very small, the S and P polarization component of wavefront 8 will merge again when they are refracted by surface 27, forming wavefront 9. Focusing lens 10 collimates the beam 9 into beam 11. Focusing lens 12 focuses the beam 11 into the photodetector 14, after passing through polarizer or analyzer 13, where the beam interferes. The interferometric signal 40, the measurement signal 41 is sent into phasemeter 24. The output signal of phasemeter 24 represents the phase difference between reference beam 15 and measurement beam 9.

In order to get the absolute flying height of the slider 28, a zero flying height has to be defined before the measurement. First, slider 28 is loaded, and made to contact with surface 27. Then, the transparent disk 25 starts rotating. At the same time, the phasemeter 24 starts counting the phase difference between signal 41 and 40. The phase difference obtained when the disk rotates at a very low speed gives the zero flying height. The phase difference obtained when the disk rotates at a full speed gives the flying height. From the phase change, the displacement of the slider can be derived from formula:

$$25 \quad \Delta\phi = \left(\frac{2\pi}{\lambda}\right)2h \cos\theta$$

where  $h$  is the spacing between disk surface 27 and ABS of slider 28.  $\theta$  is the incident angle of beam 8, and  $\lambda$  is the wavelength of the laser beam.

Referring to Figure 2A, the linearly polarized beam 51 having a frequency of  $f_o$  from the laser source 50 will expand in diameter as well as be smoothed after passing through a spatial filter 52. The beam 53 passes through acousto-optical modulator 54. When beam 53 is incident on the acousto optic modulator 54 at Bragg's angle, two orthogonally polarized beams, zero order beam 56 and the first order beam 55 having a frequency difference between them, are obtained at the output aperture of 54. In figure 2A, beam 55 has S polarization while beam 56 has P polarization. The frequency of beam 55 is modulated as  $f_o + f_c$ , where  $f_c$  is the center frequency of acousto-optical modulator 54 and  $f_o$  is the frequency of the laser beam 53. The frequency of beam 56 will remain the same as initial beam 53. Since beams 55 and 56 have orthogonal polarization, when they pass through a polarized beam splitter 57, beam 55 will be deflected, and beam 56 will pass through. The beam 56 is then directed into another polarized beam splitter 60 and passes through it. The deflected beam 55 will be directed into polarized beam splitter 60 by mirror 58 and 59. The beam splitter 60 and the deflecting mirror 58 or 59 are aligned such that the beams 55 and 56 merge together, forming beam 2. After obtaining beam 2, the beam can also be filtered.

Another preferred embodiment of source 1 is shown in Figure 2B. Here the laser source 50 is a Zeeman laser generator. A Zeeman laser generator provides a linearly polarized beam 51, where there is a frequency difference between the two orthogonally polarized beams. Beam 51 is led into spatial filter 52. At the output of 52, a laser beam is obtained having the same characteristics of beam 2.

Figure 3A is the typical structure of a spatial filter. Objective lens 60 focuses the laser beam 51 into a tiny spot in the micro meter range. Pinhole 62 acts as a filter, filtering the spatial noise contained in the laser beam. After passing through the pinhole 62, the scattered beam 61 is smoothed into beam 63. Thus, the diverged beam 63 is collimated by a collimating lens 64. The objective lens and the pinhole are carefully selected so that a smooth beam can be

obtained. Once the objective lens has been decided, the diameter of the laser beam 2 is determined by the focal length of collimating lens 64. Figure 3B illustrates the working principles of the spatial filter. A single mode fibre can be used to replace the pinhole. The fibre has the same function as pinhole, and better filtering effectiveness can be obtained.

The embodiment shown in Figure 1, takes the reference optical path directly from source 1. Another preferred embodiment is as shown in Figure 5, where the reference beam is made to pass through an optical path next to that of the measuring beam. As the reference beam and measurement beams travel nearly the same optical path, this embodiment can provide improved measurement accuracy. Non-polarization beam splitter 6 splits the beam 2 into two parts. Wavefront 8 is incident on the disk surface at oblique angle  $\theta$ , and the surface 27 transmits the P polarization component and reflects the S polarization component of wavefront 8. Thus, the surface 27 acts as the reference surface for the flying height test. The S polarization wavefront reflected back by the surface 27 passes through transparent disk 25 and is refracted by the surface 26. The P polarization component of wavefront 8 is refracted by the surface 27 and falls on the air bearing surface (ABS) of the slider 28. It is then reflected back from the ABS, passes through the transparent disk 25 and is refracted by the surface 26. As the disk-slider spacing is very small, the S and P polarization components of wavefront 8 will merge again when they are refracted by surface 27, thereby forming wavefront 9. Focusing lens 10 collimates the beam 9 into the beam 11. Focusing lens 12 is used to focus the beam 11 on to the photodetector 14, after passing through the polarizer or analyzer 13. The interferometric signal 40, the measurement signal, is sent into phasemeter 24. Mirror 42 directs the beam 15 into transparent disk 25, striking on the disk surface 26 at an angle  $\varphi$ . Angle  $\varphi$  is slightly larger or less than oblique angle  $\theta$ . Therefore, beam 17 will be completely reflected back at disk surface 27 or at the object surface 28, instead of being split into two polarization beams as what happens to the beam 8 which is

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incident to disk surface 26 at oblique angle  $\theta$ . Focusing lens 16 having the same specification as the lens 7 focuses beam 15 into a tiny laser spot on the surface 27 or 28. The alignment of the measurement and reference beams 8 and 17, respectively, are such that they focus on the same point on the surface 27 or 28.

5       Figure 6 shows the relationship of the two laser beams and the relative position of the two laser spots focused from beam 17 and beam 8. After being reflected back completely from surface 27 or 28, beam 17 is refracted by disk surface 26 into beam 18. Focusing lens 19 collimates the beam 18. The lens 21 focuses it into the photodetector 23 after passing through the polarizer or analyser 10 22, where the two orthogonal polarized components of beam 18 interfere. Interferometric signal 41 is sent into phasemeter 24, serving as the reference signal. As reference the beam passes along an optical path very close to that of the measurement beam, the errors introduced by the high-speed rotating disk, disturbance from external environment, etc., can be compensated effectively.

15     Embodiments shown in Figures 1 and 5, can measure the spacing at a single position of the slider ABS each time. If the spacing of more than one point is necessary, the slider controller 30 drives the slider 28 accordingly. The measurement step described above has to be repeated at each measurement point.

20     Other preferred embodiments of this invention are illustrated in Figures 7 and 8, which provides a beam scanning function that can access any point on the ABS of slider 28 and the rotating glass disk. The optical system and working process of embodiment shown in Figure 7 is similar to that of the embodiment shown in Figure 1, except that the polarized beam splitter is replaced by an acousto-optical deflector 3, which can scan the beam in both X and Y axes, and 25 the focusing lens 7 and 10 are replaced by scanning lens or achromatic lens 57 and 60. The crystal of the acousto optic deflector 3 is made such that the input beam to the acousto optic deflector includes both S and P polarization and the output beam includes zero order beam 4 and first order beam scanning beam 5 which both have S and P polarization states. The first order beam 5 from the acousto

optic deflector 3 is used as the scanning measurement beam. The zero order beam 4 has the same characteristics as the beam 2. The zero order beam 4 of deflector 3 is directed into focusing lens 21. Beam 4 then passes through polarizer 22 so that the beam interferes and the interference signal 41 is captured by the photo detector 23. The interferometric signal 41, the reference signal detected by photodetector 23, is sent into phasemeter 24. First order beam 5 is focused by scanning lens or achromatic lens 57 on to the object surface 28. Beam 5 strikes the disk surface 26 at oblique angle  $\theta$ . The incident angle of beam 58 to disk surface 26 is maintained as oblique angle  $\theta$  during the scanning.

Figure 9A shows the working principles of the scanning lens. The deflector, scanning lens and the measured target have to be placed according to the forward working distance (FWD) and backward working distance (BWD) of the scanning lens. The scanning lens will make all the scanning beams parallel to each other and focus the scanning beam into a tiny spot. Moreover, the scanning lens makes all the scanning beams focus onto a flat plane, which maintains the measuring spot in focus during the scanning measurement. In this embodiment, the deflector 3, scanning lens 57 and the transparent disk have to be placed according to the forward working distance (FWD) and backward working distance (BWD) of scanning lens 57, as shown in Figure 10.  $L_1 =$  FWD of scanning lens 57.  $L_2 + L_3 =$  BWD of scanning lens 57. Beam 58 is refracted by disk surface 26, changed into beam 59. Scanning lens 60 is used to change the diverging beam 59 into collimated beam 11. All the scanning beams converge at a single point, by placing disk surface 27, scanning lens 60 and focusing lens 20 according to the FWD and BWD of the scanning lens 60. As shown in Figure 10,  $L_4 + L_5 =$  BWD of scanning lens 60, and  $L_6 =$  FWD of scanning lens 60. If an achromatic or focusing lens is used in place of scanning lens, the FWD and the BWD will be equal to the focal length of the achromatic or focusing lens. If focusing or achromatic lens are used, the position accuracy may not be as accurate as scanning lens. Focusing lens 12 focuses the collimated beam 11 into one small spot falling

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on to detector 14. Before detector 14, a polarizer causes the two orthogonal polarized components of beam 11 to interfere. Interferometeric signal 40, the measurement signal, from detector 14 is sent to phasemeter 24.

Another preferred embodiment of the scanning flying height tester is shown in Figure 8. The optical system and working process of Figure 8 is similar to that of embodiment described in Figure 7, except that the reference beam is made to scan and pass through an optical path very close to that of the scanning measuring beam. The first order beam 5 from acousto-optical deflector 3 follows the same optical system as that of the embodiment illustrated in Figure 7. Zero order beam 4 of the deflector 3 is blocked by a beam blocking mechanism 100. The reference beam is obtained from the scanning first order beam 5 by using a non-polarizing beam splitter 101 and directing the beam into lens 16 with mirror 42. This beam passes through an optical system the same as that of beam 17 described in the embodiment shown in Figure 5.

Figure 11 to Figure 14 show preferred embodiments of the present invention using micro-collimated laser beams. In these embodiments, the beam 102 coming out of source 1 contains two orthogonally polarized laser beams with a frequency difference between them. Moreover, the diameter of beam 102 is in the range of micrometers. Source 1 of the present embodiments are the same as that described in Figure 2. Figure 3A shows the layout of a spatial filter. In these embodiment a micro-lens is used as the collimating lens 64. Therefore, a collimated beam with diameter in the range of micrometers can be obtained at the output of spatial filter or fiber optics by using a micro collimating lens.

Referring to Figure 11, beam 102 is split into two parts, beam 15 and beam 8 by a non-polarization beam splitter 6. The two orthogonal polarized components of beam 15 are made to interfere by passing through polarizer 22. The interferometric signal 41 detected by photodetector 23 is sent to phasemeter 24. Signal 41 is used as a reference signal. Beam 8 is incident upon the disk surface 26 at oblique angle  $\theta$ . The S and P polarization components of the beam 8

are split at disk surface 27. The P polarization component is reflected back by the ABS of slider and S polarization component of beam 8 is reflected back by disk surface 27. The two reflected polarization beams merge when they are refracted by disk surface 26 into beam 9, since the measured spacing is very small. The  
5 two orthogonally polarized components of beam 9 are made to interfere by passing through a polarizer 13. The interferometric signal 40 detected by photodetector 14 is sent into phasemeter 24.

Referring to Figure 12, beam 102 is split into two parts beam 15 and beam 8 by non-polarization beam splitter 6. Mirror 42 directs the beam 15 into the  
10 transparent disk 25, striking the disk surface 26 at an angle  $\varphi$ . Angle  $\varphi$  is slightly larger or less than the oblique angle  $\theta$ . Therefore, beam 17 will be completely reflected back at disk surface 27 or at the slider surface 28, instead of being split into two polarization beams as happens to the beam 8 which is incident on disk surface 26 at oblique angle  $\theta$ . Beam 18 is directed to the photodetector 23 and is  
15 made to interfere by passing through polarizer or analyzer 22. The interferometric signal 41, the reference signal detected by photodetector 23, is sent to phasemeter 24. Beam 8 is incident on the disk surface 26 at oblique angle  $\theta$ . The S and P polarization components of the beam 8 are split at disk surface 27. The P polarization component is reflected back by the ABS of slider and the S  
20 polarization component of beam 8 is reflected back by disk surface 27. The two reflected polarization beams merge when they are refracted by disk surface 26 into beam 9, since the measured spacing is very small. The two orthogonally polarized components of beam 9 are made to interfere by passing through a polarizer 13. The interferometric signal 40, the measurement signal detected by  
25 photodetector 14, is sent into phasemeter 24.

Referring to Figure 13, beam 102 passes through collimating lens 32 and is incident on the acousto-optical deflectors. The zero order beam 4 of deflector 3 is deflected by mirror 42 and it is used as reference beam. The two orthogonal polarized components of beam 4 are made to interfere by passing through

polarizer 22. The interferometric signal 41 detected by photodetector 23 is sent to phasemeter 24. Signal 41 is used as reference signal. Referring to Figure 9B the acousto optic deflector 3 is placed in-between two focusing or collimating lenses such that the distance between the two focusing lenses 32 and 33 is equal to the  
5 sum of the focal length of the lens 32 and 33. The scan field can be increased by either placing the acousto optic deflector 3 close to the lens 32, or by using large focal lengths for lenses 32 and 33. This optical system will produce collimated and parallel scanning beams 8 in X and Y directions. Beam 8 is incident on the disk surface 26 at oblique angle  $\theta$ . The S and P polarization components of the  
10 beam 8 are split at disk surface 27. The P polarization component is reflected back by the ABS of the slider, and the S polarization component of beam 8 is reflected back by disk surface 27. The two reflected polarization beam remix, when they are refracted by disk surface 26 into beam 9, since the measured spacing is very small. The two orthogonally polarized components of beam 9 are  
15 made to interfere by passing through a polarizer 13. Lens 12 will focus the scanning beam 9 into the photo-detector 14. The interferometric signal 40, measurement signal detected by photodetector 14, is sent into phasemeter 24.

Referring to Figure 14, beam 102 pass through collimating lens 32 and is incident on acousto-optical deflector 3. Blocking means 100 blocks the zero order  
20 beam 4 from the deflector 3. The first order beam 5 passes through collimating lens 33. Collimating lens 33 and collimating lens 32 have the same focal length. Lenses 32 and 33 and deflector 3 are placed according to the focal length of the lenses 32, 33. The combination of collimating lens 32, acousto-optical deflector 3 and collimating lens 33 provides a parallel scanning beam 5, as shown in Figure  
25 9B. Beam 5 passes through a non-polarizing beam splitter 101, which divides the scanning beam 5 into two beams, beam 8 and beam 15, with either equal or different intensity. Beam 8 is incident an the disk surface 26 at oblique angle  $\theta$ . The S and P polarization components of the beam 8 are split at disk surface 27. The P polarization component is reflected back by the ABS of slider and S

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polarization component of beam 8 is reflected back by disk surface 27. The two reflected polarization beams merge when they are refracted by disk surface 26 into beam 9, since the measured spacing is very small. Lens 12 focuses the scanning beam 9 into the photodetector 14. The two orthogonally polarized components of beam 9 are made to interfere by passing through a polarizer or analyzer 13. The interferometric signal 40, measurement signal detected by the photodetector 14, is sent into phasemeter 24. The zero order beam 4 is blocked by beam blocking mechanism 100. Mirror 42 directs the reference beam 15 into transparent disk 25, striking the disk surface 26 at an angle  $\varphi$  (beam 17). Angle  $\varphi$  is slightly larger or less than the oblique angle  $\theta$ . Therefore, beam 17 will be completely reflected back at disk surface 27 or the surface 28 of the object, instead of being split into two polarization beams as happens to the beam 8 which is incident on disk surface 26 at oblique angle  $\theta$ . Lens 20 focuses the scanning beam 9 into the photodetector 23. The two orthogonally polarized components of beam 18 are made to interfere by passing through polarizer or analyzer 22. The interferometric signal 41, the reference signal detected by photodetector 23, is sent to phasemeter 24.

### Second Embodiment of the Present Invention

The second embodiment of the present invention increases the resolution of the system without reducing the spot size of the focused beam on the object.  
20 Referring to Figure 16, the measurement beam 11 passes through a diaphragm or slot 200, which allows only a certain portion of the beam 11 to pass through and the rest of the beam is blocked. A small portion of the measurement beam 201 is focused on the measurement photo detector 14 by the focusing lens 12 after passing through an analyzer or polarizer 13. A smaller size for slot 200 will result in higher resolution for the system. By this method, a portion of the object 25 smaller than the focal spot size of the beam can be measured. For example, if the focal spot size on the object is 10 micrometer and the collimated beam size of the beam 11 is 10mm, the photo detector measures the average of the entire focused

spot on the object. In order to measure the 1-micrometer area of the object by using 10 micrometer focused spot size, only 1mm of the collimated beam 11 will pass through the diaphragm, and the rest of the beam will be blocked. In this case, the photodetector provides the average of 1-micro meter on the object, which corresponds to the 1mm of the beam 11 passing through the diaphragm 200. With this method, the resolution of the object area to be measured can be increased without reducing the focal spot size of the beam on the object.